

Toward remote sensing with broadband terahertz waves

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Abstract This paper studies laser air-photonics used for remote sensing of short pulses of electromagnetic radiation at terahertz frequency. Through the laser ionization process, the air is capable of generating terahertz field strengths greater than 1 MV/cm, useful bandwidths over 100 terahertz, and highly directional emission patterns. Following ionization and plasma formation, the emitted plasma acoustic or fluorescence can be modulated by an external terahertz field to serve as omnidirectional, broadband, electromagnetic sensor. These results help to close the “terahertz gap” once existing between electronic and optical frequencies, and the acoustic and fluorescence detection methodologies developed provide promising new avenues for extending the useful range of terahertz wave technology. Our experimental results indicate that by hearing the sound or seeing the fluorescence, coherent detection of broadband terahertz wave at remote distance is feasible.

Keywords terahertz, air, plasma, fluorescence, acoustic

1 Introduction

Terahertz electromagnetic waves, defined as the frequency region between 0.1 and 10 terahertz on the electromagnetic spectrum, have demonstrated remarkable usefulness for imaging and chemical identification with the ability to penetrate many optically opaque barriers. Photon energies at these frequencies are relatively small (meV), which means the radiation is non-ionizing and therefore considered biologically innocuous. With the growing list of applications and demand for terahertz technology, there is a need to develop innovative terahertz sources and detectors that can overcome existing limitations in power, bandwidth, and operating range. Although terahertz

radiation has demonstrated unique and exceptional abilities, it has also presented several fundamental challenges. Most notably, the water vapor absorption of terahertz waves in air at habitable altitudes is greater than 100 dB/km. There is an immediate push to utilize the material and vapor identification abilities of terahertz radiation, while extending the effective distances over which the technology can be used. Remote terahertz detection, until recently, was thought to be impossible due to the high water content in the atmosphere, limited signal collection geometries, and solid state materials necessary for generation and detection.

2 Terahertz air photonics

Terahertz wave generation from intense laser-plasma interaction in air was first reported by Hamster et al. in 1993 [1]. At the time, single color (800 nm) sub-picosecond laser pulses were used, and the generation process was attributed to the ponderomotive force inside the plasma. In 2000, Cook and Hochstrasser reported that higher intensity terahertz radiation could be emitted from laser-induced gas-plasma excited with both a fundamental pulse (800 nm) and its second harmonic (400 nm) [2]. The terahertz wave emission mechanism was attributed to the four-wave mixing (FWM) nonlinear optical process. At that time, several other groups became interested in this topic. Among them, Bartel et al. reported terahertz wave generation from gas-plasma with peak electric fields higher than 100 kV/cm, indicating promising applications of the gas-plasma terahertz wave source [3]. However, the physical process for terahertz wave emission remained under debate. In order to identify the basic mechanism, coherent control experiments were performed which verified that FWM could be used to explain the terahertz wave generation process in a gas-plasma [4]. More importantly, using the FWM approximation, the detection of broadband pulsed terahertz waves with a laser-induced

gas-plasma was successfully predicted and experimentally demonstrated [5].

2.1 Generation and detection of terahertz waves in air

Terahertz air photonic systems differentiate themselves from other terahertz time-domain spectrometers by using ambient air or selected gases for the generation and detection of broadband pulsed terahertz waves [4–7]. Figure 1(a) illustrates the schematic diagram for a terahertz air biased coherent detection (THz-ABCD) spectroscopic system in both transmission and reflection mode. Figure 1(b) illustrates plasma formed after focusing a high-energy laser pulse into the air.

A Ti:Sapphire regenerative amplifier is typically used as the laser source. Such a laser delivers laser pulses with millijoule pulse energy, femtosecond pulse duration, 800 nm center wavelength, and kilohertz repetition rate. The beam is split into pump and probe beams using a beamsplitter. The pump beam is focused through a beta-barium borate (β -BBO) crystal to produce the second harmonic at 400 nm. The mixed fundamental and second harmonic beams (ω and 2ω respectively) generate the ionizing plasma spot (center-right of Fig. 1(b)) that emits intense, directional, and ultra-broadband terahertz radiation through a third-order nonlinear process [2]. Although FWM cannot completely describe the complex physical details [8–11], it remains a convenient framework for experimental results due to its simplicity. After interaction with a sample, the remaining terahertz energy and optical probe beam are recombined at the detection region, where an electric bias (E_{bias}) is applied to create a second harmonic local oscillator for coherent detection through DC-field-induced second harmonic generation [12]. Figure 2 shows that the terahertz field is proportional to the

intensity of the fundamental pulse (ω) above the ionization threshold for lower intensities, and is proportional to the square root of the second harmonic pulse (2ω) [13]:

$$E_{\text{THz}} \propto \chi^{(3)} \sqrt{I_{2\omega}} I_{\omega}. \quad (1)$$

It is important to note that this relationship is only valid for relatively low peak laser power intensities, since FWM is an approximation invalid when the intensity is high. At higher laser power intensities, the plasma electron density increases and reduces the Debye length. In other words, there is a screening effect that no longer yields a linear relationship between the THz amplitude and the peak laser power.

Similar to the widely used generation and detection of terahertz waves in electro-optic crystals by second order optical nonlinearity [14–16], terahertz waves can be detected by the third order optical nonlinearity in air or other selected gases [5,6]. Figures 3(a) and 3(b) plot terahertz waveforms and spectra detected with laser-induced air-plasma using THz-ABCD in comparison with the conventional electro-optic method with an electro-optic ZnTe crystal as the sensor. Using air as the sensor, the spectrum from 0.3 to over 30 terahertz sufficiently covers the “terahertz gap”. Using shorter laser pulses, terahertz peak fields may exceed 1 MV/cm, and the spectrum may extend beyond 120 terahertz [17]. As a comparison, the DC breakdown threshold for air is about 30 kV/cm.

The use of air to sense pulsed terahertz waves is a measurement of the terahertz field induced optical second harmonic light generated through a third-order nonlinear process that has been investigated extensively in the previous literature [12,18,19], and therefore details will not be presented here. The measured second harmonic intensity can be expressed as

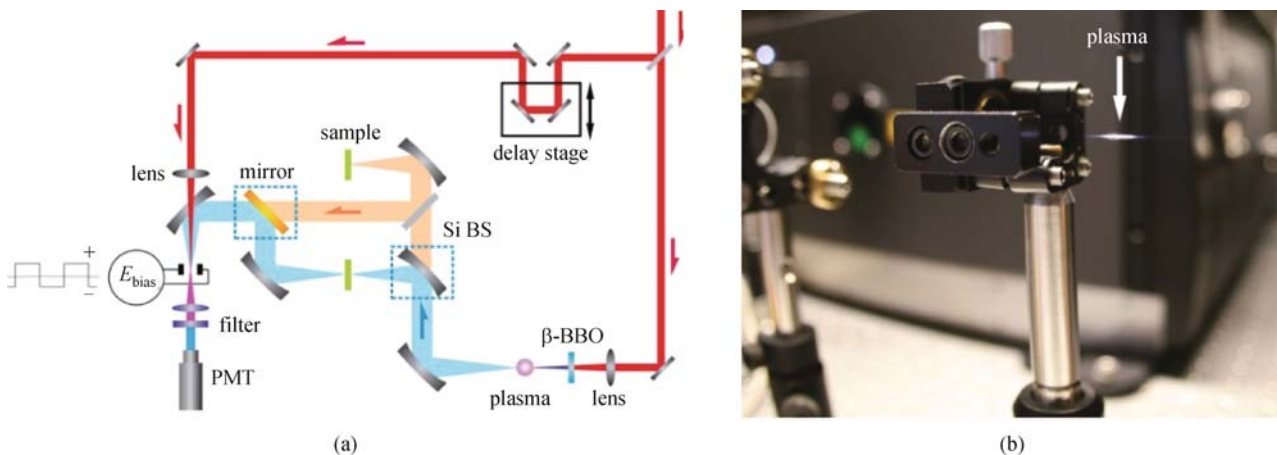


Fig. 1 (a) Schematic diagram of a THz-ABCD spectroscopic system in both transmission and reflection mode. The system can be converted from transmission to reflection mode by taking out the mirrors indicated with an enclosing dashed box. PMT: photomultiplier tube; BS: beamsplitter; β -BBO: beta-barium borate; (b) photograph of laser-induced air-plasma created after focusing the optical beam from left to right through a lens (left) and mounted nonlinear crystal (center) used for second harmonic generation. The bright horizontal line emits an intense, highly directional terahertz field to the right

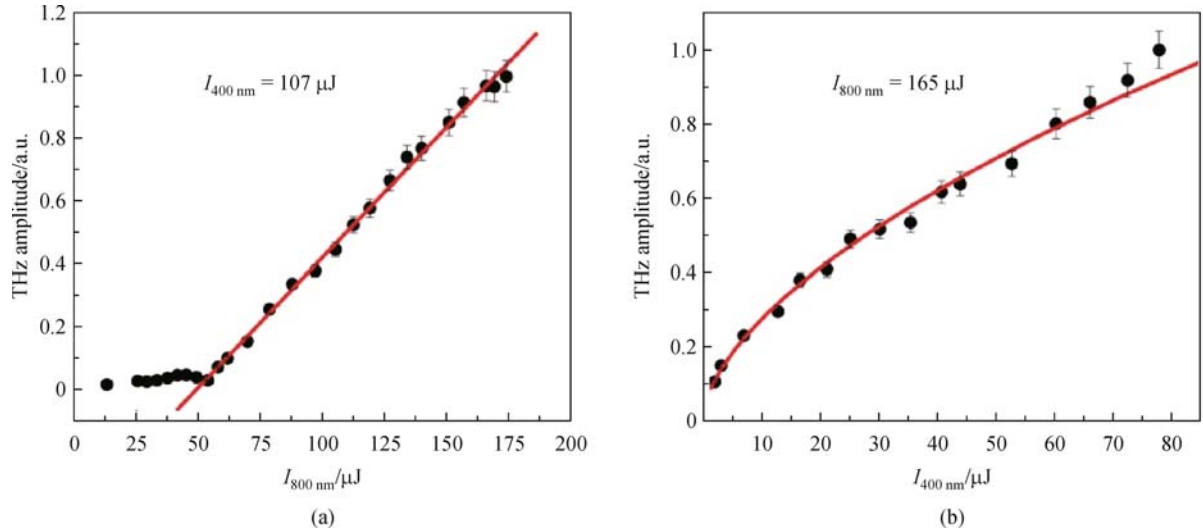


Fig. 2 (a) Dependence of terahertz field on fundamental (ω) pulse energy, with fixed second-harmonic (2ω) pulse energy; (b) dependence of terahertz field on second-harmonic pulse energy, with fixed fundamental pulse energy. The solid line and curve are the linear and square-root fits, respectively. Reprinted figure with permission from Ref. [4]

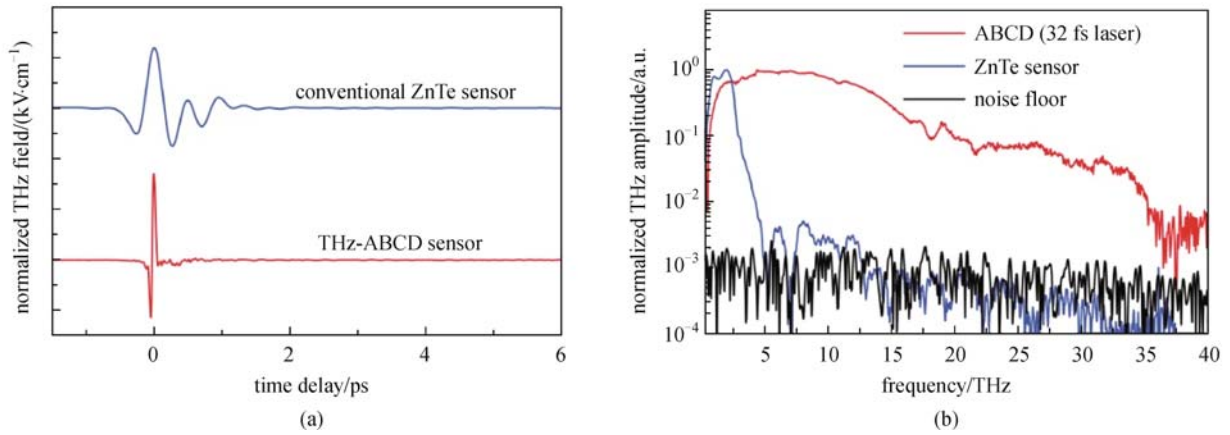


Fig. 3 (a) Time-resolved terahertz signals generated and detected using dry nitrogen gas as compared to conventional electro-optic (EO) crystal detection in ZnTe. The probe beam for air detection has energy of 85 μJ and pulse duration of 32 fs; (b) corresponding spectra after Fourier transformation

$$I_{2\omega}(\tau) \propto 2[\chi^{(3)}I_{\omega}(t)]^2 E_{\text{bias}} E_{\text{THz}}(t-\tau). \quad (2)$$

Equation (2) is the key description for detection. The linear dependence of $I_{2\omega}$ on E_{bias} indicates heterodyne detection when E_{bias} is treated as a local oscillator. The field-induced second harmonic signal $I_{2\omega}$ is quadratically proportional to $\chi^{(3)}$ and $I_{\omega}(t)$, and linearly proportional to E_{bias} and $E_{\text{THz}}(t-\tau)$.

Figure 4(a) illustrates this concept, where terahertz and optical pulses are focused collinearly together, with their polarization aligned parallel to the modulated E_{bias} field. The second harmonic induced by E_{bias} acts as the local oscillator for heterodyne detection [12] that can be used to perform phase sensitive detection. Figure 4(b) plots the detected second harmonic intensity as a function of

normalized third order nonlinear susceptibility $\chi^{(3)}$ along with a quadratic fit [6,20]. We can see that C_6H_{14} provides more than 243 times the sensitivity compared with N_2 or air. Using gases with larger $\chi^{(3)}$, elevated pressure (effective $\chi^{(3)}$ is proportional to the number of molecules), and higher probe pulse energy can help to optimize the sensitivity of the air-plasma detector [6].

2.2 Terahertz air photonic system electronics

The broad range of applications for air photonic systems has already yielded commercially available systems that utilize air-plasma as the source. One example is a recent system released by Newport Corporation [21]. The Newport system utilizes air-plasma for terahertz wave genera-

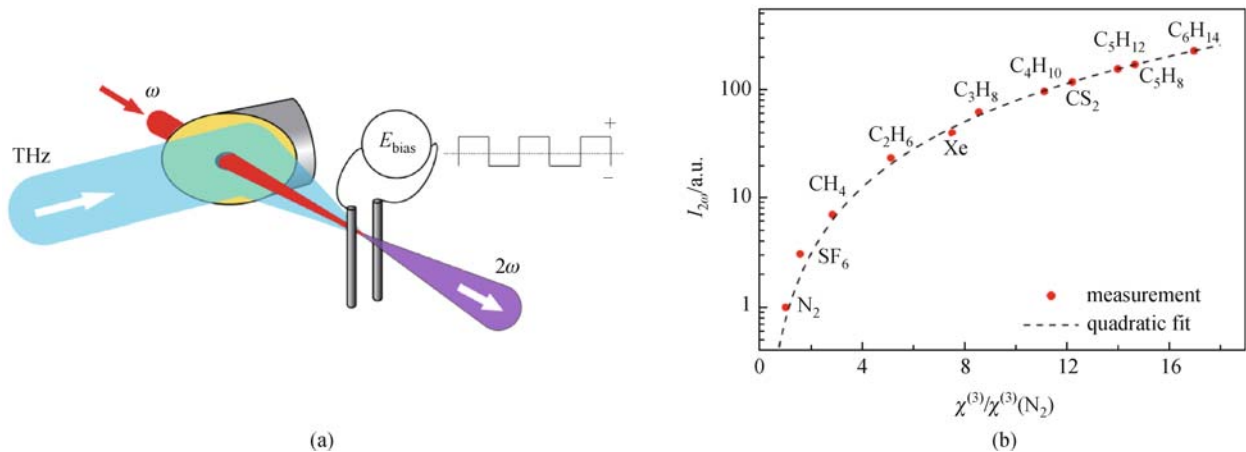


Fig. 4 (a) Basic concept of THz-ABCD: electrodes are placed at the geometric focus of collinearly focused terahertz and optical probe beams with a variable time delay. Second harmonic light is induced from the terahertz field and the local bias field E_{bias} . Modulating E_{bias} allows for heterodyne detection for enhanced sensitivity; (b) measured second harmonic intensity vs. third order nonlinear susceptibility $\chi^{(3)}$. All $\chi^{(3)}$ are normalized with respect to nitrogen. Data in (b) courtesy of Dr. Xiaofei Lu

tion, however the detectable bandwidth is limited to 3 terahertz since an electro-optic ZnTe crystal is used for detection. While for the nonlinear four wave mixing process, it is necessary to supply a high field local oscillator for coherent detection. This can be achieved electronically in two ways. The first method is to produce a high voltage square wave, triggered by an input signal, such as the laser transistor-transistor logic (TTL) output signal. The second method is to produce a high voltage pulse, where the timing of the pulse becomes important relevant to when the optical pulse arrives between the pair of biasing electrodes. The following sections describe square and pulsed high voltage modulator designs that we successfully prototyped, one of which was later developed into a commercially available product sold by Zomega Terahertz Corporation.

2.2.1 Square wave high voltage modulator

A strong local oscillator electric field is necessary for

coherent terahertz wave detection through air-photonics as seen from Eq. (2), making the supporting high voltage electronics an invaluable tool in the system. For high voltage modulation, there are several things that need to be considered. Firstly, the more sensitive digital and analog control circuitry need to be isolated from high voltage potentials to minimize cross talk that can potentially interrupt circuit functionality. Secondly, attention to packaging and safety become important factors since large voltages are present at all times on the board. Thirdly, it is necessary to engineer the switching of these high voltages on the board without damaging the internal circuitry. As shown in the 3D rendered prototype in Fig. 5, the digital, analog, and high voltage electronics were all housed within a small aluminum box. The front panel uses a backlit liquid crystal display (LCD) to display voltage outputs, and a digital rocker switch to adjust the amplitude, phase, and modulation frequency.

The rear panel contains a heat exhaust fan, a CH1, CH2, and COM banana plug connection for interfacing the

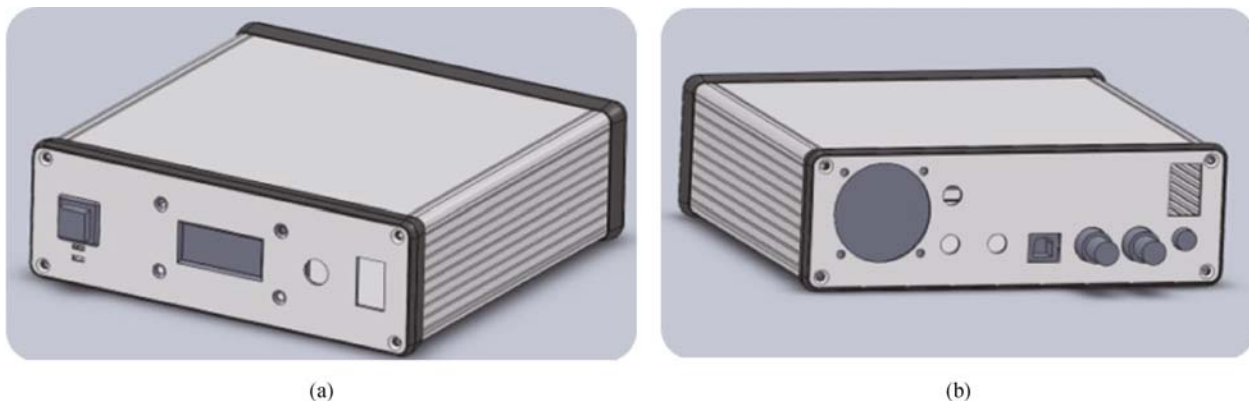


Fig. 5 3D-rendered Solidworks model of high voltage square wave modulator

switched high voltage output to a pair of electrodes in the THz-ABCD system. A universal serial bus (USB) interface is installed for optional communication and control of amplitude, phase, and frequency via a computer host. Additionally, the rear panel contains a TTL input and output reference signal for phases sensitive detection using a lock-in amplifier, a 12 volt power supply port for powering the device, and an ON/OFF toggle switch for immediate on and off control of the unit.

2.2.1.1 High voltage switching

The DC high voltage (HIGH V) is created using a commercially available DC to DC converter sold by EMCO that steps a 12V DC input up to the kilovolt level. Voltage switching was accomplished by implementing a full bridge N-channel metal-oxide-semiconductor field-effect transistor (MOSFET) design as depicted in Fig. 6.

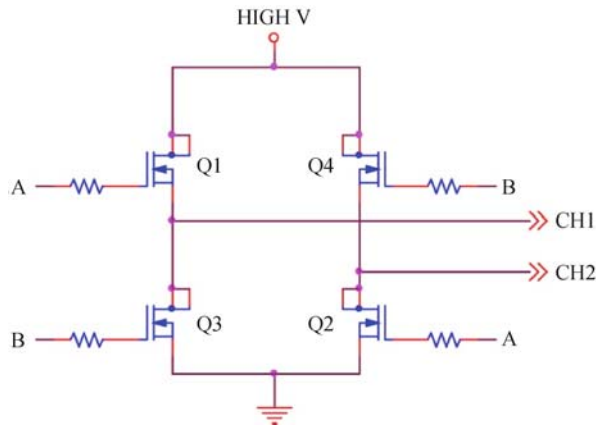


Fig. 6 N-channel MOSFET full bridge topology used for switching voltages with drive signals A and B

When the “A” signal is held high, MOSFETs Q1 and Q2 are turned on and CH1 becomes the potential of HIGH V, while CH2 becomes the potential of ground. Alternatively, when “B” signal is held high, MOSFETs Q3 and Q4 are turned on and CH1 becomes grounded while CH2 becomes the potential of HIGH V. If the CH1 and CH2 connections are connected to a pair of electrodes, the potential between them is simply their difference as shown in Fig. 7. This creates an alternating electric field between them at a selectable division of the input TTL signal, which in our case is determined by the amplified laser repetition rate of 1 kHz.

For lower voltages, the circuit design in Fig. 6 is adequate. However, since we desire to switch voltages on the order of several kilovolts, the commercial availability of high drain-to-source breakdown voltage field-effect transistors (FETs) becomes limited. In order to switch these kilovolt voltages, it becomes necessary to distribute the

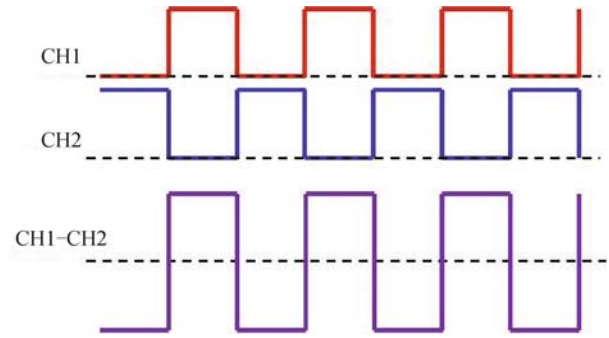


Fig. 7 Alternating voltage bias using an N-channel MOSFET bridge

voltage over a series of MOSFETs, switching them simultaneously to prevent breakdown. This was accomplished using an audio transformer with four separate 1:1 coils. The input signal at one coil is transformed into a potential across the other three windings, allowing for three separate MOSFET gates to be driven simultaneously. Varistors were used as protection circuitry to prevent any high voltage transient spikes that could potentially develop across the drain to source of the MOSFET if the gates are not switched at precisely the same time.

2.2.1.2 Operational testing

After construction, the device was tested at its maximum operating potential. Figure 8 shows the experimental test of the single-sided output using a 1/1000 resistor divider to protect the oscilloscope probe breakdown voltage of 300 V. It can be seen that high voltage is switched relative to the TTL trigger input, meaning that each laser pulse receives a modulated bias at 1/2 the input frequency (500 Hz in our case). This means that the electric field orientation between the electrodes alternates between each pulse passing through the site of the electrodes.

It is important to note that the measurement made here is single-sided, meaning the potential is between CH1 and ground. If we looked at the potential between CH1 and CH2, we would see twice the potential of the single sided measurement with an alternating electric field direction as depicted in the lower portion of Fig. 7. The alternating field is used as a local oscillator for coherent terahertz wave detection. The prototype, later developed into a commercial product, is shown in Fig. 9, and is available through Zomega Terahertz Corporation [22].

2.2.2 Pulsed high voltage modulator

The alternative for creating a high voltage local oscillator for use in air photonics is to create short pulses of high voltage. The advantages of using a pulsed system are not only size reductions, since compact high quality factor

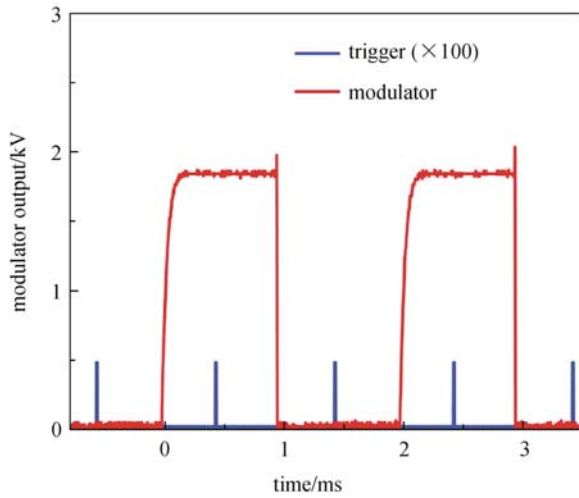


Fig. 8 Square wave high voltage modulator operating at maximum output voltage as determined by the DC-DC converter. The laser TTL output is sent to the modulator and a voltage divider is used to monitor the CH1 output. When operating with electrodes, the total output potential is CH1–CH2, twice that shown

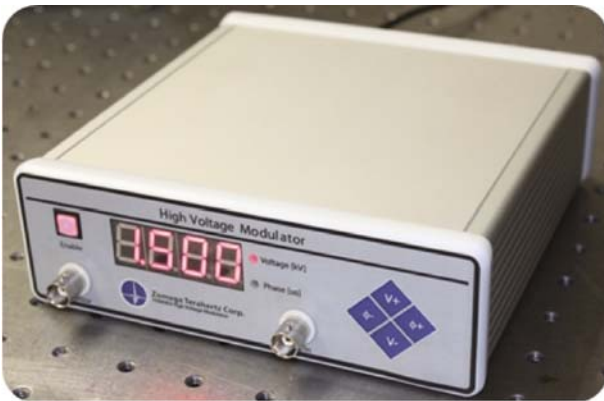


Fig. 9 Commercialized high voltage square wave modulator sold through Zomega Terahertz Corporation

transformers can be used to replace large DC-DC converters, but also the possibility to instantaneously generate high voltages with low level voltage inputs. This means there are only very short periods of time that have high voltage potentials on the board. The disadvantage of this system is that timing becomes very important, since the high voltage pulse must be present at the site of the electrodes during the passage of the optical pulse. A 3D rendering of the pulsed high voltage modulator prototype is shown in Fig. 10.

The pulsed system front panel has three main elements. From left to right: amplitude/phase selection switch with amplitude/phase indicator light emitting diode (LED); an LCD display; increment/decrement rocker switch for adjustment of phase and amplitude, and phase lock indicator LED. On the back, the prototype has a USB interface, a TTL input and output reference, a 12 volt power jack with an ON/OFF toggle switch, and a port for connection of the high voltage leads that interface to the electrodes.

2.2.2.1 Digital circuitry

For this system, a Texas Instruments MSP family microcontroller was used to perform functions such as analog to digital conversion and display of the amplitude and phase readings. A Xilinx computer programmable logic device (CPLD) was used to implement a digital phase-locked loop (PLL) to synchronize the laser TTL input signal with the internal oscillator used for adjusting the timing delay of the output pulse. The digital PLL was implemented in software as shown in Fig. 11.

A frequency divided output from a voltage controlled oscillator (VCO) and the laser TTL input are used as the input clock sources of the flops. If the clocks are not raised high simultaneously, a small pulse is sent to either the Freq_Up or Freq_Dn outputs of the Xilinx chip before the outputs of the flops are cleared. If the clock for both flops is raised simultaneously, the flops are not cleared and the



Fig. 10 3D rendered Solidworks model of pulsed high voltage modulator prototype

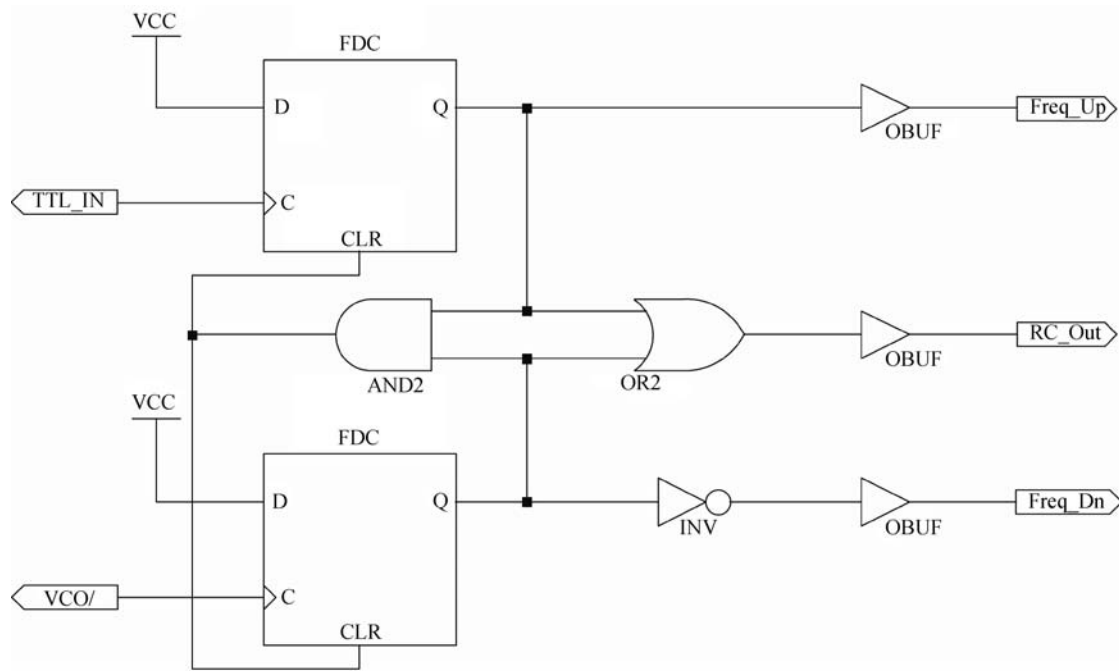


Fig. 11 Digital implementation of phase locked loop in a Xilinx CPLD to synchronize digital circuitry timing to laser trigger signal

resulting output is balanced, making RC_Out logic low which causes the phase lock LED to illuminate.

Once the digital circuitry clock has been synchronized to the reference laser trigger, the delay between an internally generated 1 kHz pulse train and the input trigger signal is controlled by using a 16-bit loadable cascading bidirectional binary counter (DB16X1) with a 16-bit cascading adder/subtractor (ADSU16). The adder has a constant time value loaded at startup to compensate for the time the optical pulse must propagate through the air to reach the electrodes. Additional phase adjustments are made by "tickling" the SETFREQ pin on the MCU to increase or decrease the delay between the input trigger and the output high voltage pulse. The MODENABLE pin on the MCU is reserved for controlling either increment or decrement functions. The phase delay adjustment digital circuitry implemented in the Xilinx CPLD is shown in Fig.12. Once the 16 bit counter (CB16CE) counts up to the desired delay value, the COMP16 comparator output goes high to initiate the output pulse. If the value of the delay timing is changed, the flash memory in the MCU is updated with the new value so that this timing is saved for the next time the device is turned on.

2.2.2.2 Analog circuitry

The external analog circuitry interfacing to the CPLD can be seen in Fig.13. The small voltage pulses from Freq_Up or Freq_Dn result in either charging or discharging of the

capacitor C67, which determines the set voltage of the voltage controlled oscillator for synchronizing the internal oscillator to the reference signal.

In order to produce the high voltage pulses, the same technique is borrowed from the square wave modulator bridge design relating to Fig. 6. By using two separate pulses at the input of a transformer, it is possible to make the potential drop across the transformer look like twice that of the input voltage. In addition, by controlling the relative timing between the two input pulses, it is possible to change the output polarity of the high voltage spike as seen in Fig.14. Here a 1/1000 resistor divider is used to look at the output of the transformer that will be connected to the biasing electrodes.

Similar to the method for generating an alternating electric field with the square wave modulator in Fig. 7, it is important that the electric field alternates for the pulsed system. In order to flip the polarity of the high voltage pulse, the CPLD digital logic is programmed to alternate between the two timing scenarios shown in Fig. 14. A phase-locked output of the unit is shown in the experimental data presented in Fig. 15. It is this pulse train output that can be adjusted accurately in phase such that the peak of each high voltage pulse is aligned with the precise time that the combined optical and terahertz pulses exist between the electrodes in the THz-ABCD system.

Since the optical pulse lasts for only femtosecond time duration, even if the electric field pulse duration is on the order of nanoseconds, the voltage seen by the optical field

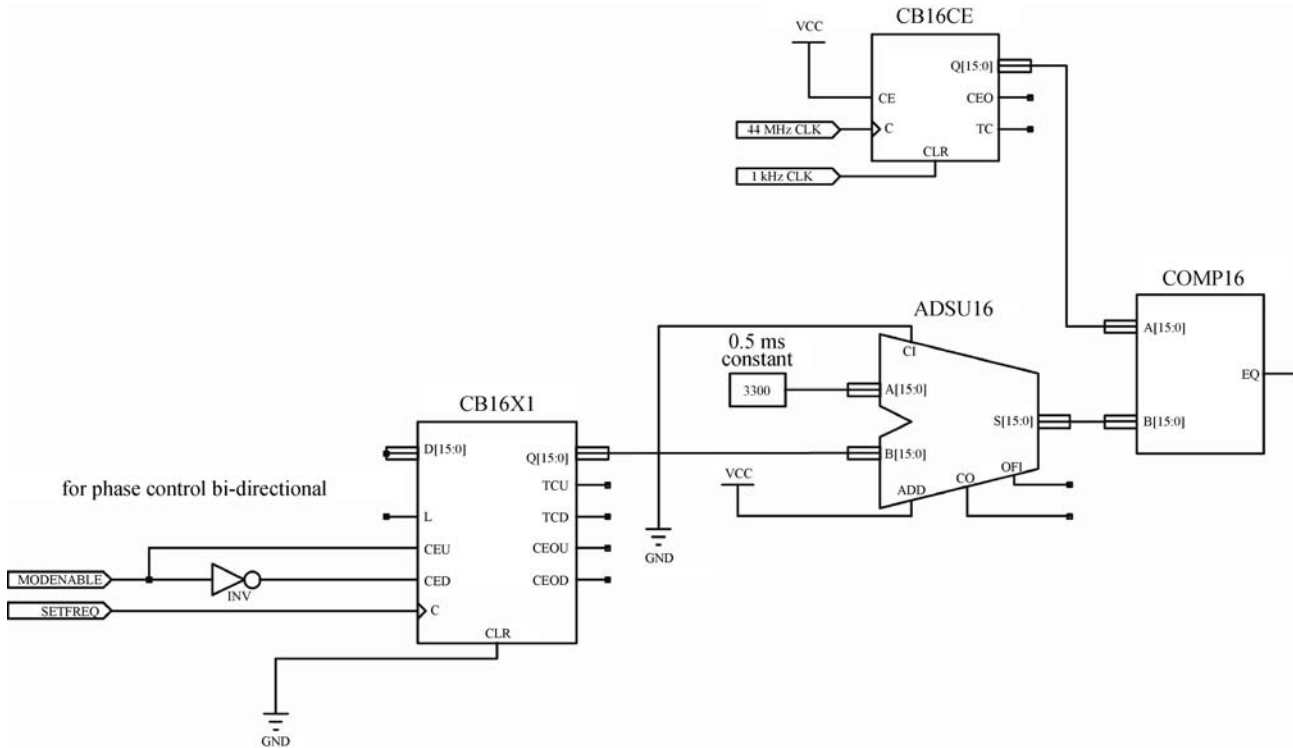


Fig. 12 Electronic pulse phase control circuitry implemented in the Xilinx CPLD. CB16X1: 16-bit loadable cascaded bidirectional binary counter; CB16CE: 16-bit cascaded binary counter; ADSU16: 16-bit cascaded adder/subtractor; COMP16: 16-bit Identity Comparator

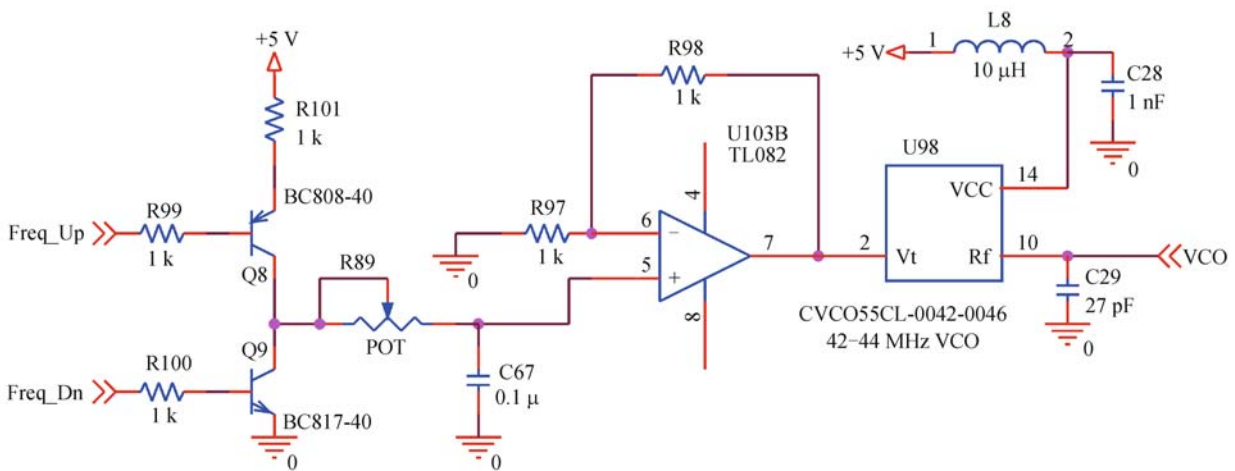


Fig. 13 Analog circuitry interfaced to Xilinx CPLD for phase locked loop

will appear to be constant, meaning any following oscillations are irrelevant to the detection process and can actually benefit the user when finding the initial system timing.

2.2.3 Summary

Two high voltage modulator prototypes were developed to

be used with the terahertz air photonic system that utilizes nonlinear photomixing of terahertz and optical photons, in combination with a high-strength local oscillator field, to perform coherent terahertz wave detection in air. It can be seen that there are benefits to each system. The square wave modulator electronics design is by far more simplistic, since the electronic pulse timing is unimportant (phase can be set to anything other than right at the

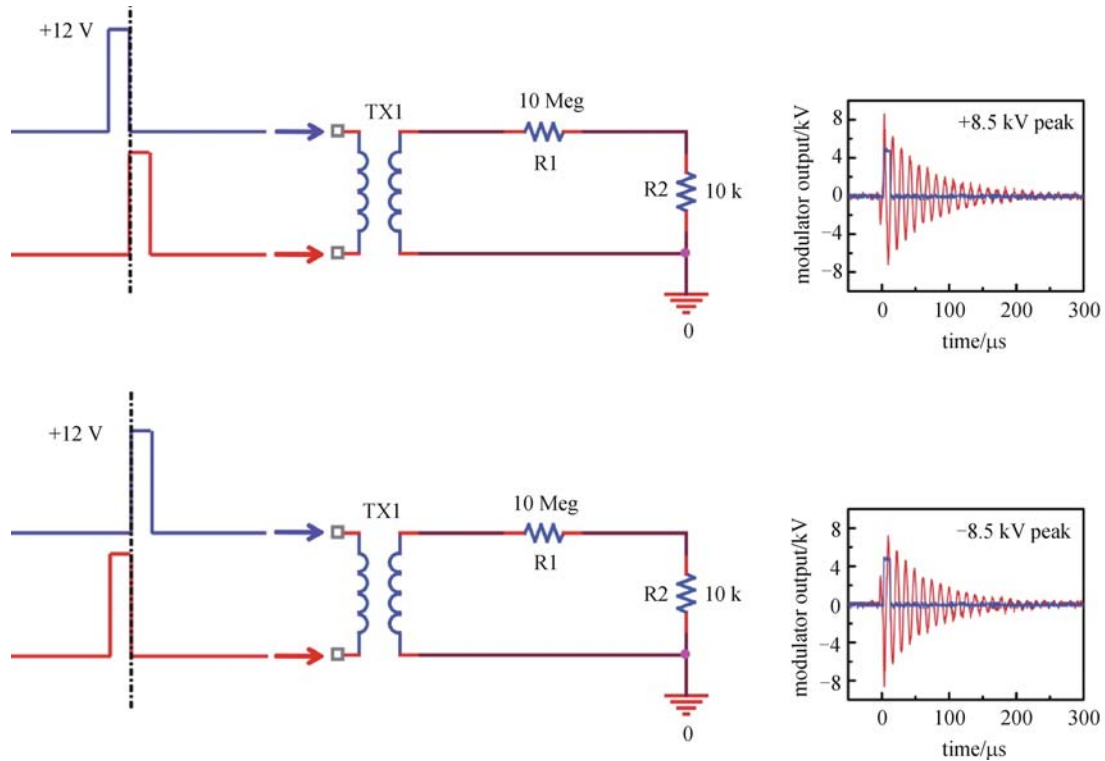


Fig. 14 A compact, high Q -factor, high turns-ratio transformer is pulsed using the output from the MOSFET bridge. The polarity of the high voltage output pulse is determined by the input pulse timing

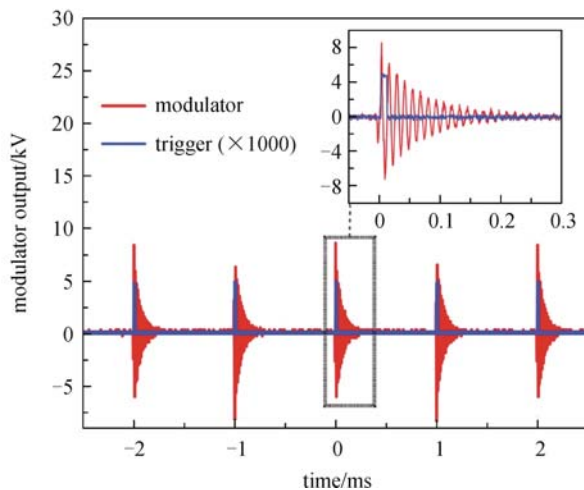


Fig. 15 Phase-locked output of pulsed high voltage modulator showing filed polarity altering between each trigger from the reference

transition). Although the pulsed system requires more complex circuitry, it has a more compact form factor, and results in higher possible voltage outputs due to its transient nature. It is also considered a safer device since the nanosecond high voltage transients are only present at the output for short periods of time rather than the constant high voltages that exist on the circuit board at all times with the square wave modulator.

2.3 Terahertz detection through air-plasma fluorescence

Due to the composition of gasses in air, as free electrons in the plasma relax to lower energy states through the recombination with ions, visible fluorescence is emitted which can be modulated by an external electromagnetic pulse. The external field influences the number of fully ionized states through collisional excitation of bound high-lying Rydberg states, yielding information about the external instantaneous field in the form of fluorescence changes. Therefore, terahertz signals can be detected indirectly through observation of the terahertz-radiation-enhanced-emission of fluorescence, a technique nicknamed (THz-REEF) [23]. It is therefore possible that terahertz spectroscopic “fingerprints” of materials can be encoded into fluorescence (300–450 nm) wavelengths, advantageous due to their transparency during atmospheric propagation and low detectible signal levels using highly sensitive optical sensing equipment. In a previously conducted THz-REEF experiment, shown in Fig. 16(a), a terahertz pulse propagated through the plasma and the fluorescence was measured by a spectrometer. By increasing the kinetic energy of electrons through terahertz-field acceleration in the plasma, as illustrated in Fig. 16(b), fluorescence emission could be enhanced. Figure 16(c) shows the nitrogen fluorescence spectra with and without the terahertz field imposed on the gas-plasma.

When two-color pulses (800 and 400 nm) are super-

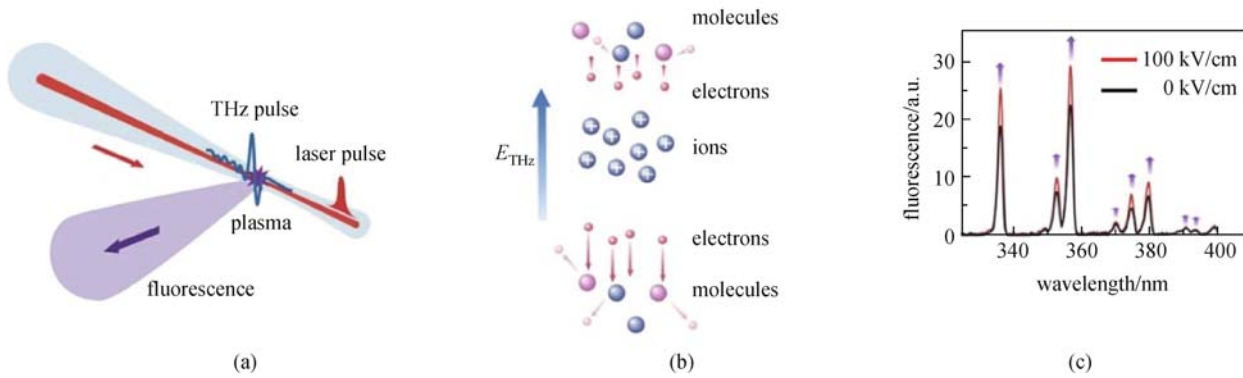


Fig. 16 (a) Experimental geometry for THz-REEF from air-plasma using a single-color laser pulse excitation; (b) electron acceleration in the terahertz field and collision with neighboring molecules; (c) THz-enhanced fluorescence spectra of nitrogen gas-plasma under influence of 100 kV/cm peak field. © IEEE, reprinted, with permission from Ref. [24]

posed to form a plasma, the ionized electrons' net drift velocity becomes a function of the relative phase between the pulses [8]. Electron motion can be symmetric, parallel, or anti-parallel to the terahertz wave polarization by changing the relative phase of the pulses. Once the terahertz pulse arrives, electrons are driven to move faster (if $E_{\text{THz}}(t)$ is anti-parallel to the initial velocity) or slower (if $E_{\text{THz}}(t)$ is parallel). Figure 17(a) shows the time-resolved air-plasma fluorescence for the parallel, symmetric, and antiparallel electron drift velocities as the terahertz pulse interacts with the plasma.

In each scenario, there is fluorescence enhancement, but each contains unique “features” from either the increase, constant, or decrease in electron velocity (and therefore energy transfer) by the terahertz field [25]. Figure 17(b) shows the coherent terahertz waveform revealed in the fluorescence by subtracting the parallel curve from the

antiparallel curve. The THz-REEF signal thus allows for terahertz wave coherent detection, meaning air-plasma fluorescence can also indirectly give information regarding a material.

2.4 All air-plasma terahertz spectroscopy

Among many important applications of terahertz radiation in science and industry, it is fair to say that terahertz time domain spectroscopy (THz-TDS) has become a highlight due to its exceptional ability to excite vibrational and rotational modes within organic materials, including but not limited to explosive compounds [26]. Although terahertz spectroscopic “fingerprinting” has proved to be an exceptional method for material characterization [27,28], these classifications require solid state materials such as electro-optic crystals or electrodes that must be

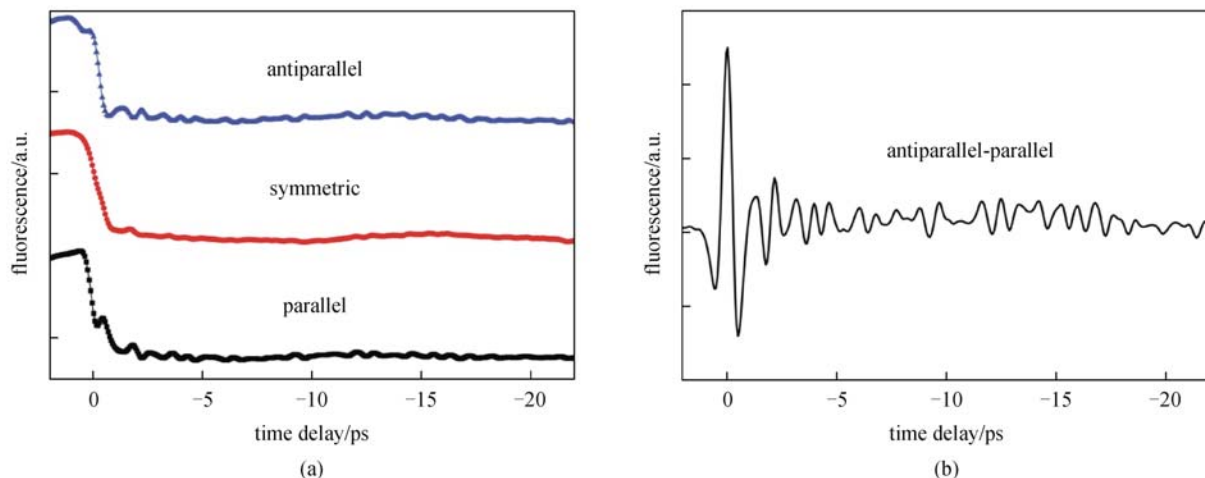


Fig. 17 (a) Time-resolved air-plasma fluorescence enhancement from terahertz wave interaction with antiparallel, symmetric, and parallel electron drift velocities with respect to the laser field, controlled by changing the relative phase between the ω and 2ω optical pulses; (b) subtracting the parallel curve from the antiparallel curve removes the incoherent energy transfer by electrons after inelastic collisions and scattering in random directions. This reveals the terahertz waveform in the form of fluorescence modulation. The optical pulse leads the terahertz pulse in time for delay $t_d < 0$

used in conjunction with the laser pulse for generation and detection [12,14,15,29]. Furthermore, current terahertz detection methods require the detector to collect information of the terahertz wave in the forward propagating direction; information regarding the terahertz transient is unable to be retrieved in the backwards direction. It is also impractical to send terahertz waves directly to the sample through the atmosphere due to fundamentally large water vapor attenuation [30]. For these reasons, terahertz spectroscopic measurements have all taken place under purged nitrogen environments, or at extremely short distances where the operator remains exposed to the potential hazards under study. Remote terahertz spectroscopy remains somewhat a “holy grail”, since it would enable non-invasive material identification from a safe distance.

In this section, an “all air-plasma” terahertz spectroscopy system is introduced, that encodes explosive signatures of Nitroguanidine (NG), 2,4-Dinitrotoluene (2,4-DNT), and Cyclotetramethylene tetranitramine (HMX) into the nitrogen fluorescence emitted from a bichromatic laser-induced plasma filament using fluorescence detection principles discussed previously. Since the plasma filament serves as both the terahertz emitter and detector, terahertz pulse detection is no longer restrained by electrodes, solid state materials, or forward signal collection; showing the feasibility for conducting remote terahertz spectroscopy. We show that broadband terahertz pulses emitted from a plasma filament source, and the omnidirectional nitrogen fluorescence from a two-color plasma filament can carry spectroscopic information regarding terahertz-material interaction.

2.4.1 Prior efforts for remote terahertz wave sensing

In 2009, Dai and Zhang demonstrated remote terahertz wave generation by focusing two optical pulses into air at 17 meters from the last optic to form a plasma that emitted broadband pulses of terahertz radiation [31]. An in-line phase compensator, preceding the large diameter focusing mirror, was used to mechanically stabilize and adjust the phase between the fundamental and second harmonic laser pulse [32]. In 2010, Wang et al. demonstrated a similar measurement obtaining terahertz pulse energies larger than 250 nJ [33]. Both demonstrations show the ability for generating intense terahertz radiation at remote distances; however, the problem remains carrying coherent information regarding the terahertz electromagnetic pulse back to the user. More recently, as proof of concept, we showed that single-cycle terahertz pulse information could be encoded into laser-induced plasma nitrogen fluorescence and acoustic waves [25,34,35]; however, these demonstrations both used a solid state LiNbO_3 crystal for the terahertz wave source, and therefore the system was restricted to local distances with a system bandwidth less than 3 terahertz.

2.4.2 Experimental setup

Here all air-plasma terahertz spectroscopy is demonstrated, utilizing nitrogen fluorescence encoding, which is performed using laser plasmas for both the terahertz wave emitter and detector as would be necessary for remote operation. Figure 18 shows the pump-probe experimental layout. Of the total 700 μJ system input pulse energy, 70% was sent to the pump to generate terahertz waves through two-color ionization of the air [2,8,36]. The remaining 30% was used to generate a plasma detector from which the nitrogen fluorescence was monitored. A 100 μm thick type-1 β -BBO crystal was used to generate second harmonic pulses from the 80 fs 500 μJ optical pump pulses. The terahertz pulse energy was estimated to be 50 nJ (limited only by laser input energy) using a calibrated pyroelectric detector. Field strengths of 40 kV/cm were produced from the generation plasma as measured by electro-optic sampling techniques [14]. In comparison, over 300 nJ pulse energies were generated through the tilted pulse front method used for initial plasma acoustic and fluorescence encoding demonstrations. An in-line phase compensator [32] controlled the relative phase between the 800 and 400 nm pulses, and moreover the electron trajectory inside the bichromatic field-induced probe plasma [8].

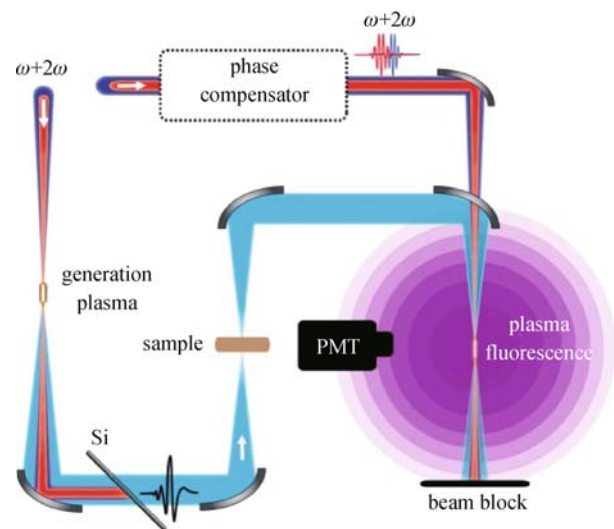


Fig. 18 “All air-plasma” terahertz spectroscopy system. Air-plasma filaments are used for both generation and detection of the terahertz electromagnetic radiation. (Light blue: terahertz), (Red: 800 nm pulse), (Blue: 400 nm pulse), (Purple: nitrogen fluorescence). Nitrogen fluorescence emitted from the probe plasma carries the encoded terahertz pulse information

Terahertz radiation from the air-plasma source was collected and refocused through a pair of 3” off-axis parabolic mirrors (OAPM) for testing samples in transmis-

sion geometry. The transmitted terahertz energy was refocused collinearly with the two color probe pulses using a 2" OAPM.

2.4.3 Experimental results and discussion

A photomultiplier tube with a (354 ± 10) nm filter was used to monitor the probe plasma nitrogen fluorescence at 357 nm while the delay between terahertz and optical pulses was scanned. Figure 19(a) shows the coherent terahertz pulse after decoding the nitrogen fluorescence using techniques discussed in reference [25]. A waveform in Fig. 19(a) and spectra in Fig. 19(b) of the same pulse recovered using a 100 μ m thick GaP electro-optic crystal, is showed for comparison, indicating congruency between the respective methods.

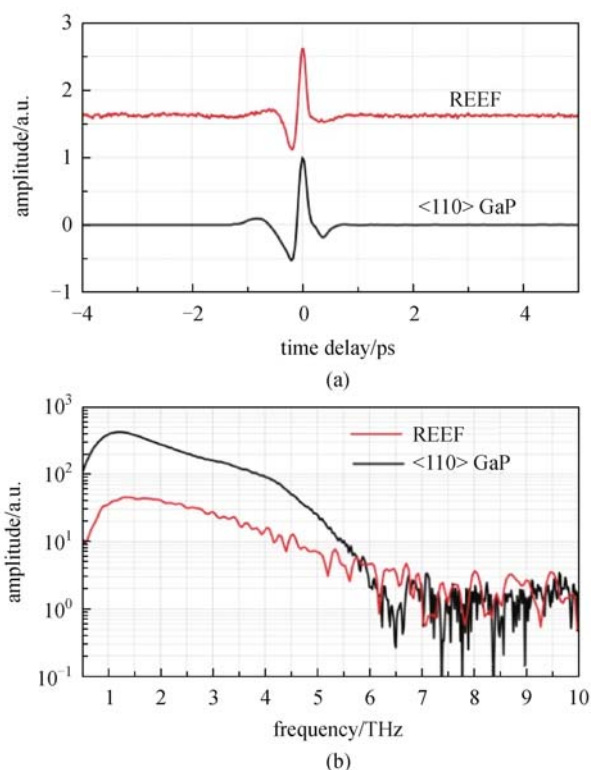


Fig. 19 (a) Terahertz pulses recovered from the radiation-enhanced-emission of fluorescence (REEF) and electro-optic sampling method using a 100 μ m thick $\langle 110 \rangle$ GaP crystal; (b) corresponding spectrum after Fourier transformation

Since the THz-REEF technique does not require solid state materials for detection, the useable bandwidth is not limited by material phonon resonance, but only by optical pulse duration. In order to demonstrate the broadband spectroscopic capability of this method, spectroscopic signatures of NG, 2,4-DNT, and HMX were encoded into the nitrogen fluorescence, using experiments in which the samples of these three explosive materials interacted with a

pulsed terahertz signal. The respective electro-optic measurements were performed to validate the reliability of the method. Although not specifically necessary, measurements described here were performed under dry nitrogen purged conditions to elucidate explosive sample absorbance signatures and increase the system signal-to-noise ratio (SNR) for reduced averaging times. Figures 20 (b) and 20(d) compare the absorbance information using fluorescence encoding and electro-optic sampling methods.

The spectroscopic features of all chemical compounds are sufficiently resolved by the two methods. Slight variations in the terahertz waveform and absorption signatures were expected due to small differences in sample positioning and terahertz-optical beam overlap in the plasma or electro-optic crystal, however, the absorption peak locations show good agreement between the respective methods and the existing literature values [37,38].

Each sample was prepared by uniformly mixing micrometer grain size polyethylene powder containing 20% of the explosive compound. The samples were compressed at 9 metric tons for 3 minutes and were all less than 1 mm thick. For these measurements, sample preparation was important due to laser power limitations and therefore available terahertz pulse energy. A compromise between the system SNR and sample absorbance had to be made. Samples containing larger than 20% chemical concentrations undoubtedly produced more noticeable absorption features; however, this came at the penalty of reduction in transmitted terahertz energy and therefore a substantial decrease in the fluorescence measurement SNR. For this reason, all chemical concentrations were limited to 20%, which allowed for more than 50% transmission of the terahertz peak electric field.

3 Terahertz enhanced acoustics

Until recently, the generation and detection of terahertz waves using laser air photonics has taken place on an optical table bench, where a combination of carefully positioned optics and electronics have been fused to perform broadband terahertz spectroscopy. In this part, a new concept is discussed that aims to push the capabilities of table-top air photonic terahertz systems beyond the lab bench to a remote site, where carefully positioned optics and electronics can no longer be used. By “listening” to laser-induced plasma, it becomes feasible to carry information of terahertz waves through the atmosphere in an isotropic geometry. Although many technical challenges remain, this unique technique presents another large step toward realizing a remotely operational terahertz spectrometer; opening new scientific directions and opportunities for electromagnetic sensing.

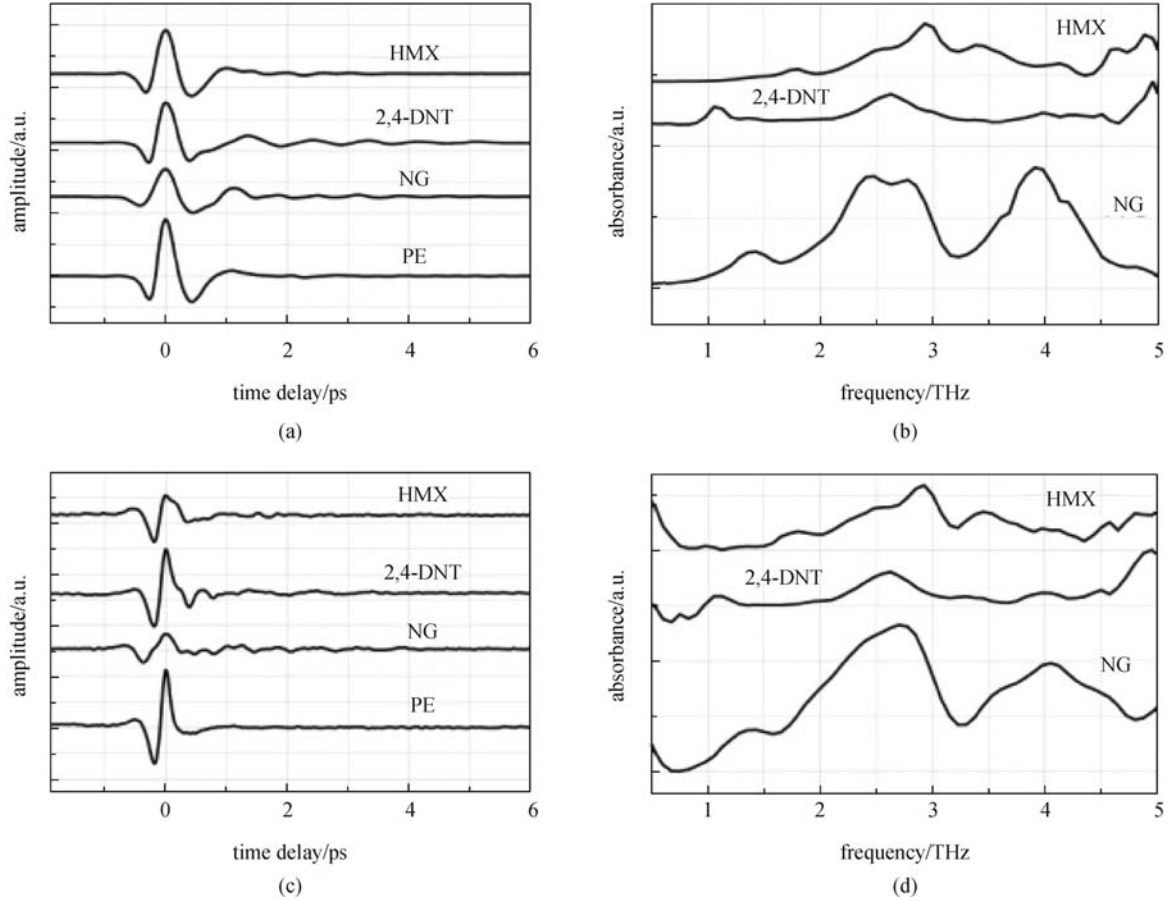


Fig. 20 (a) Terahertz waveforms for pellet samples NG, 2,4-DNT, and HMX containing 20% chemical mixed with polyethylene obtained using electro-optic sampling; (b) absorbance signatures corresponding to samples in (a); (c) identical samples and corresponding waveforms obtained using radiation enhanced emission of fluorescence (REEF) encoding; (d) absorbance signatures corresponding to samples in (c). All curves are offset for clarity

3.1 Theoretical model

Under the irradiation of intense optical fields, such as high-power femtosecond laser pulses focused into air, the molecules are ionized, meaning free electrons are released from their parent molecules once the laser field overcomes the atomic Coulomb potential. After being ejected from the atoms or molecules during the leading part of the laser pulse, the electrons are accelerated by the remainder of the laser pulse and drift away from their parent ions. In the intense laser field excitation, the electron temperature is usually much higher than the temperature of the neutral particles (mostly molecules in air and ions whose mass are generally thousands of times larger than the electron mass). Before the electron-ion recombination, these “hot” electrons collide with the neighboring “cold” molecules and transfer some portion of kinetic energy through inelastic electron-molecule collisions in the following nanoseconds [39]. The subsequent translational motion of the molecules gives rise to the creation of a shock wave, which then relaxes into an acoustic wave [40–42].

While when a terahertz wave irradiates the plasma, the terahertz field can modify the plasma acoustic pressure by changing the electron velocity and therefore kinetic energy transfer to the plasma. To study the influence of terahertz waves on plasma acoustics, a theoretical model containing laser-induced photoacoustics and kinetics of electrons and molecules in the terahertz field is constructed here. Acoustic wave propagation in the presence of a heating source can be written as [43]

$$\left(\nabla^2 - \frac{1}{c_s^2} \frac{\partial^2}{\partial t^2}\right)p(r,t) = -\frac{\beta}{C_p} \frac{\partial H(r,t)}{\partial t}. \quad (3)$$

Here, the sound velocity, c_s is assumed to be constant after thickening of the shock, for which the wave is restored to the linear region [44,45]. The β and C_p are the isobaric volume-expansion coefficient and heat capacity per unit mass at constant pressure respectively, and $p(r,t)$ is the acoustic pressure (deviation from atmospheric). $H(r,t)$ is the heating function, defined as the rate of the heat transfer from electrons into molecular translational energy,

where

$$H(r,t) = n_e E_T h(r,t) \propto (n_e m_e v_e^2 / 2) h(r,t).$$

The $h(r,t)$ term is determined by the nature of the energy transfer process and is a complex function of gas density and laser intensity. Here, n_e is the free electron density. E_T is the total energy transferred from each electron to neighboring air molecules in the single-electron approximation, where electron-electron interaction is neglected. The solution of Eq. (3), $p(r,t)$, can be expressed as

$$p(r,t) = n_e E_T f(r,t) \propto (n_e m_e v_e^2 / 2) f(r,t), \quad (4)$$

where $f(r,t)$ can be obtained using the Green's function solution of Eq. (3), together with $h(r,t)$ [43], and its specific expression is not of much concern since only its dependence on electron temperature is of interest here.

When the plasma is subjected to an external terahertz field $E_{\text{THz}}(t)$, the acceleration of free electrons and the following electron-molecule collisions give rise to a local plasma temperature increase. This temperature increase results in the enhanced acoustic emission from the plasma. The energy transfer, E_T , is therefore increased to $E_T + \Delta E_T$ through terahertz-induced electron heating. Since the electron relaxation time, τ , at atmospheric pressure is small in comparison to the terahertz pulse duration [46], the terahertz waveform can be "segmented" into many small pieces, within which the terahertz field is considered constant. This treatment would simplify the calculation of terahertz-driven electron motion. Therefore, the pressure enhancement $\Delta p(r,t,t_D)$ can be approximated as

$$\begin{aligned} \Delta p(r,t,t_D) &= n_e \Delta E_T(t_D) f(r,t) \propto n_e m_e \sum_{i=1}^{\infty} (\Delta \vec{v}_{ei})^2 \\ &= \frac{e^2 n_e \tau}{m_e} \int_{t_D}^{\infty} \vec{E}_{\text{THz}}(t')^2 dt', \end{aligned} \quad (5)$$

where n_e can be treated as a constant since the terahertz pulse duration is much shorter than the electron-ion recombination time, which is on the scale of nanoseconds [47]. The time delay between the terahertz pulse and the laser pulse is t_D , and its sign is defined so that t_D is positive when the terahertz pulse leads the optical pulse in time, and negative when the terahertz pulse is behind the optical pulse. $\Delta \vec{v}_{ei}$ is the change of the electron velocity by the terahertz field during the time period between the $(i-1)$ th and the i th electron-molecule collision. Here, $\Delta \vec{v}_{ei} = - \int_{t_i-\tau}^{t_i} e \vec{E}_{\text{THz}}(t') dt' / m_e$. Furthermore, the magnitude of the enhancement ratio is described as

$$\frac{\Delta p}{p} = \frac{m_e \sum_{i=1}^{\infty} (\Delta \vec{v}_{ei})^2}{m_e v_e^2 / 2}, \quad (6)$$

where, for a 100 kV/cm peak terahertz field, the maximum $m_e \sum_{i=1}^{\infty} (\Delta \vec{v}_{ei})^2 = \frac{e^2 \tau}{m_e} \int_{t_D}^{\infty} \vec{E}_{\text{THz}}(t')^2 dt'$ is estimated to

be 0.3 eV in the limit of very short relaxation time (i.e., τ is much smaller than the terahertz pulse duration). The initial electron kinetic energy $m_e v_e^2 / 2$ is estimated to be several eV for the laser intensity of $10^{13} \sim 10^{14}$ W/cm² [48]. From this theoretical model, it can be seen that acoustic emission from a laser-induced plasma might serve as an electromagnetic sensor.

3.2 Experiments and discussion

According to the theoretical predictions above, we experimentally investigate the terahertz wave detection by using photoacoustics. The methods include incoherent and coherent detection.

3.2.1 Incoherent detection

In the experiment illustrated in Fig. 21(a), a single-color (800 nm, 80 fs, 110 μ J pulse energy, 1 kHz repetition rate) optical pulse was focused into the air to produce an acoustic pulse. The total laser intensity at the focus was $10^{13} \sim 10^{14}$ W/cm². Under illumination of an intense femto-second laser pulse, photoionization of the molecules takes place in the sub-picosecond time scale as the laser field overcomes the Coulomb potential binding the electrons to their parent atoms. The laser field increases the free electron temperature, T_e , to $10^4 \sim 10^5$ K, while neighboring molecules or ions have a much lower temperature, T_m [48]. In the following $10^{-8} \sim 10^{-9}$ s, T_m is gradually increased through energy transfer from collisions between hot electrons and their surrounding air molecules until thermal equilibrium is achieved [39,49]. This rise in localized gas temperature produces a shock wave that persists for a short distance [50], before relaxing into an acoustic wave [41].

The waveform of the acoustic pulse was measured with a broadband microphone (G.R.A.S 40DP). A single-cycle terahertz pulse with peak field of approximately 100 kV/cm, generated using the tilted pulse front optical rectification technique in LiNbO₃ [29], was spatially and temporally overlapped with the optical pulse. When the adjustable time delay between the terahertz pulse and optical pulse, ' t_d ' in Fig. 21(a), was negative (optical pulse preceding the terahertz pulse), a 10% amplitude enhancement of the sound pressure in the entire waveform was observed. Figure 21(b) shows the measured acoustic waveforms with and without the 100 kV/cm terahertz field incident on the plasma. The corresponding inset shows the terahertz-induced pressure enhancement in the frequency domain (up to 140 kHz) after Fourier transformation of the single-pulse waveforms.

Furthermore, a pair of wire grid polarizers, with 1000:1 extinction ratio and bandwidth from 0 to 4 terahertz, was used to determine the acoustic enhancement dependence on the terahertz wave. The angle between the first polarizer and the vertical direction, θ , is tuned, while the second

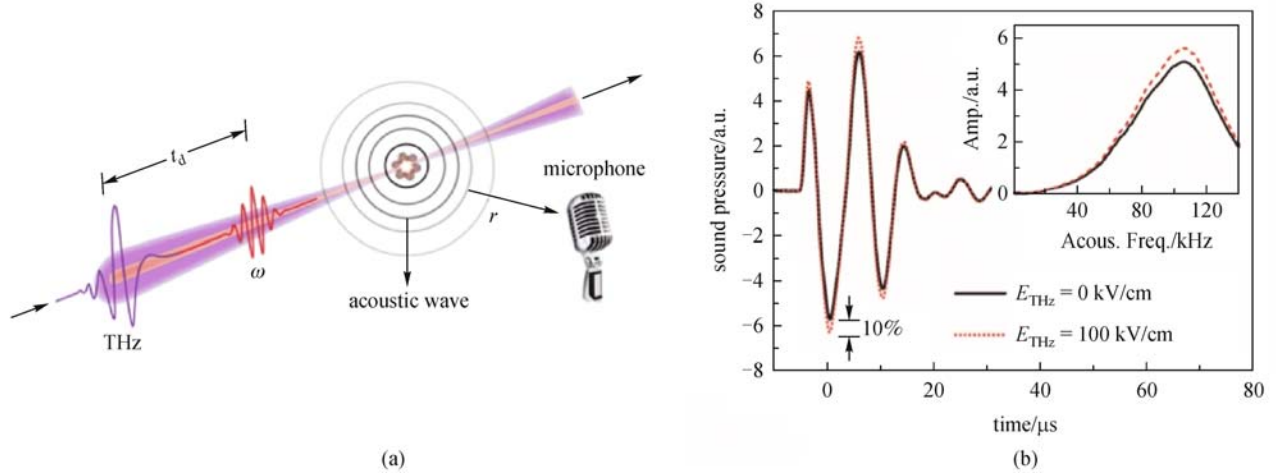


Fig. 21 (a) Experimental setup for performing terahertz enhanced acoustics using single-color femtosecond laser excitation; (b) single photoacoustic waveforms measured at 5 mm distance with (red-dashed) and without (black-solid) a 100 kV/cm terahertz field. The insert shows the acoustic spectra in linear scale. Amp.: amplitude; Acous. Freq.: acoustic frequency

polarizer is fixed at 90° and transmits the vertical component of the terahertz wave. Thus, after passing two polarizers, the terahertz wave is kept vertically polarized and the amplitude of the terahertz field is $E_{\text{THz}}\cos^2(\theta)$ and the amplitude of the terahertz intensity is $I_{\text{THz}}\cos^4(\theta)$. The measured results (red dots) and quadratic fit (dashed blue line) are shown in Fig. 22, in which the observed quadratic dependence is also consistent with the terahertz field squared term in Eq. (5).

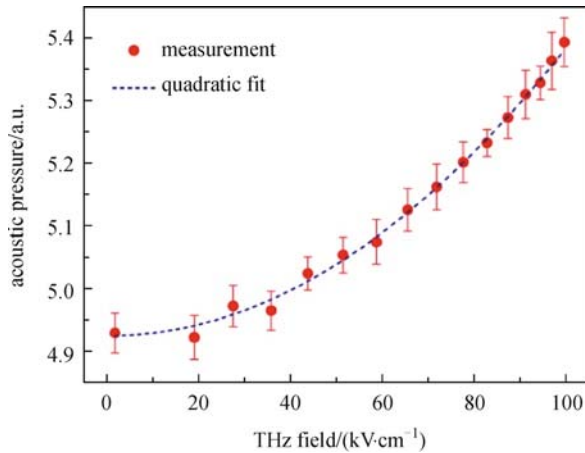


Fig. 22 Measured terahertz field dependence of acoustic pressure (red dots) at 100 kHz and quadratic fit (blue dashed line)

Besides, to study laser-induced photoacoustic dynamics under single-cycle terahertz radiation, the acoustic signal at 100 kHz was measured by varying the time delay t_d . The results are shown as the solid curve in Fig. 23. In region I, the terahertz pulse leads the optical pulse in time and there is no acoustic enhancement, because there is no interaction between the terahertz pulse and the plasma; however, when

the field of the terahertz pulse begins to interact with the plasma, a sharp rise in the acoustic signal is observed, with the period of rising time comparable to the width of a single-cycle terahertz pulse. In region II, following the rise, a slow decay of the acoustic signal on the order of nanoseconds is observed and agrees with the temporal profile of the electron density decay due to electron-ion recombination [47].

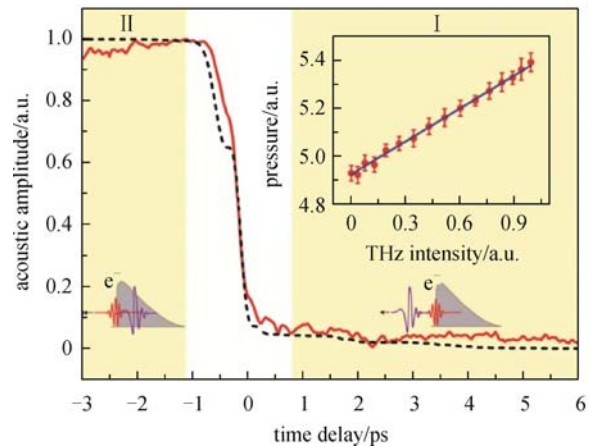


Fig. 23 Normalized pressure enhancement signal at 100 kHz as a function of time delay t_d . Region I: terahertz pulse leads the optical pulse in time; region II: terahertz pulse trails the optical pulse in time. The dashed line is the calculated signal. Inset shows the acoustic signal at 100 kHz for different terahertz intensities incident on single-color laser-induced plasma and a linear fit

Additionally, a lock-in amplifier measured the acoustic signal at 100 kHz, using the 100th harmonic of the laser repetition rate (1 kHz). The inset of Fig. 23 shows the acoustic enhancement at 100 kHz for different terahertz intensities. Good agreement between the measurement and

linear fit shows that the enhanced acoustic pressure is linearly dependent on incident terahertz wave intensity, making the plasma pressure emission useful as a detector.

Therefore, in single-color laser excitation, the terahertz-wave-enhanced acoustic pressure is quadratically dependent on the terahertz field due to the symmetrical distribution of electron drift velocity. Thus acoustic emission from single-color laser plasma can be used for terahertz wave detection. The advantages of this detection method are: 1) the omnidirectional pattern of the acoustic emission, which enables the signal collection at any direction; 2) the low attenuation of the acoustic wave in the ambient air, which makes it possible to use laser-induced plasma as a sensor to detect terahertz waves at a standoff location while sending information back to the user via acoustic waves. These merits are attractive for remote terahertz sensing; however, one disadvantage of this method is that the detection is incoherent, i.e., no phase information of the terahertz pulse can be recovered from the acoustic signal.

3.2.2 Coherent detection

Compared to the case of single-color laser excitation, the terahertz-wave-enhanced acoustic emission can be quite different if two-color laser fields, E_ω (800 nm) and $E_{2\omega}$ (400 nm), are used for plasma formation. Figure 24 shows the modified experimental layout.

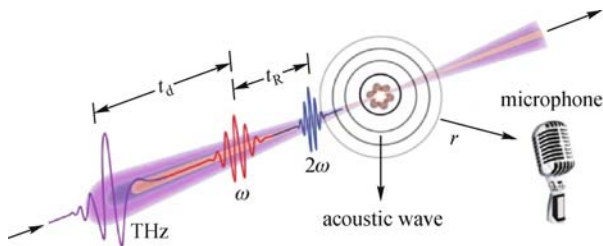


Fig. 24 Experimental schematic for the THz-enhanced acoustics using two-color femtosecond laser excitation

For E_ω and $E_{2\omega}$ laser fields aligned parallel to each other, the combined field $E_{\text{Opt}}(t)$ can be expressed as

$$\begin{aligned} E_{\text{Opt}}(t) &= E_\omega(t) + E_{2\omega}(t) \\ &= A_{\omega 0}(t)\cos(\omega t) + A_{2\omega 0}(t)\cos(2\omega t + \phi_{\omega, 2\omega}), \quad (7) \end{aligned}$$

where $A_{\omega 0}(t)$, $A_{2\omega 0}(t)$ are the envelopes of the E_ω and $E_{2\omega}$ pulses respectively. By changing the relative phase of the two optical fields, $\phi_{\omega, 2\omega}$, the drift velocity distribution and electron trajectories can be controlled [51,52].

In order to determine the optical phase dependence on the drift velocity distribution, the terahertz emission from the plasma excited by a two-color laser field is measured at different $\Delta\phi_{\omega, 2\omega}$, since the amplitude of terahertz signal is

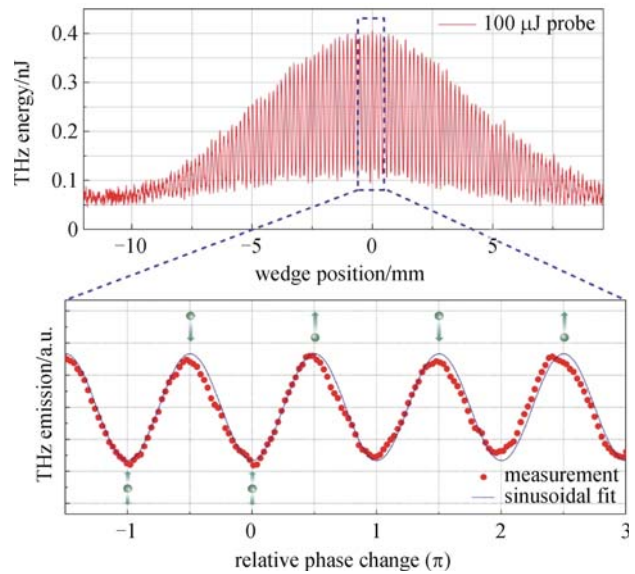


Fig. 25 Dependence of terahertz wave generation from plasma on the relative phase delay between 800 nm pulse and 400 nm pulse. The arrow refers to the electron drift direction. At the maxima of the terahertz emission, the electron drift velocity is highly asymmetric, while at the minima of the terahertz emission, the electron drift velocity is nearly symmetric

correlated to the asymmetry of the electron drift velocity [53]. The results are shown in Fig. 25 and the zoom of the figure shows the data with sinusoidal fit. We can see that, at the relative phase change $\Delta\phi_{\omega, 2\omega}$ of $\pm(2l + 1)\pi/2$ (where l is an integer), the electron drift velocity distribution is strongly asymmetric; while at the relative phase change $\Delta\phi_{\omega, 2\omega}$ of $\pm l\pi$, the electron drift velocity distribution is almost symmetric. Thereby, information of the electron drift velocity distribution is crucial for coherent control of the acoustic pressure enhancement, and knowledge of electron motion will provide new techniques for coherent terahertz wave detection.

While for the excitation of a two-color laser field, the terahertz-wave-induced pressure enhancement $\Delta p(\Delta\phi_{\omega, 2\omega})$ takes a more complicated expression including the drift velocity distribution $\rho(\vec{v}(0), \Delta\phi_{\omega, 2\omega})$ and initial drift velocity $\vec{v}(0)$ [23]:

$$\begin{aligned} \Delta p(\Delta\phi_{\omega, 2\omega}) &\propto n_e \left[\int_{-\infty}^{+\infty} \left(m_e \vec{v}^2(0) + 2m_e \vec{v}(0) \Delta \vec{v}_{ei} \right) \right. \\ &\quad \left. \rho(\vec{v}(0), \Delta\phi_{\omega, 2\omega}) d\vec{v}(0) / 2 + m_e \sum_{i=1}^{\infty} \Delta \vec{v}_{ei}^2 \right]. \quad (8) \end{aligned}$$

When a terahertz field interacts with a plasma induced by a particular relative optical phase delay between ω and 2ω (affecting the initial electron drift velocity at the time of photoionization), the electrons that experience the terahertz field are either slightly accelerated or decelerated depend-

ing on whether the terahertz field is anti-parallel or parallel to the initial momentum “kick” given to the freed electrons at birth. Scanning the delay between the terahertz and optical pulses “ t_d ” for relative delays of $-\pi/2$ and $\pi/2$ between the ω and 2ω pulses “ t_R ”, the rising enhancement curves for opposite net electron drift directions are obtained. The results are plotted in Fig. 26(a). In both cases, there is acoustic wave enhancement which results from terahertz-field induced electron heating and increased electron-electron, electron-ion, and electron-molecule collisions; however, under parallel and anti-parallel conditions, the free electrons are either decelerated or accelerated along the direction of the terahertz field, contributing to the overall acoustic emission.

Despite the complex form of Eq. (8), the difference between $\Delta p(-\pi/2)$ and $\Delta p(\pi/2)$ can be reduced to a much more simplified expression by taking the symmetry of $\rho(\vec{v}(0), \pi/2) = \rho(-\vec{v}(0), -\pi/2)$ into consideration. This eliminates the second order term of \vec{E}_{THz}^2 while only the first order term \vec{E}_{THz} is left. Using a mathematical identity and a change of variable, the first two terms of Eq. (8) evaluated at $\pi/2$ can be transformed to

$$-\int_{+\infty}^{-\infty} \left[m_e (-v'(0))^2 + 2m_e (-v'(0)) \Delta v_{ei} \right] \rho \left(-v'(0), \frac{\pi}{2} \right) \frac{d-v'(0)}{2}, \quad (9)$$

where $v'(0) = -v(0)$. From symmetry, $\rho(v(0), \frac{\pi}{2}) = \rho(-v(0), -\frac{\pi}{2})$ and Eq. (9) can be rewritten as

$$-\int_{-\infty}^{+\infty} \left[m_e (-v'(0))^2 - 2m_e (v'(0)) \Delta v_{ei} \right] \rho \left(v'(0), \frac{\pi}{2} \right) \frac{dv'(0)}{2}. \quad (10)$$

Changing back to the original variable, Eq. (8) can then be written as

$$-\int_{-\infty}^{+\infty} \left[m_e (v(0))^2 - 2m_e (v(0)) \Delta v_{ei} \right] \rho \left(v(0), \frac{\pi}{2} \right) \frac{dv(0)}{2}. \quad (11)$$

Performing the subtraction:

$$\begin{aligned} \Delta p(-\pi/2) - \Delta p(\pi/2) \\ = 4m_e v(0) \Delta v_{ei} \rho \left(v(0), \frac{\pi}{2} \right) dv(0)/2. \end{aligned} \quad (12)$$

Since $\Delta v_{ei} = -\int_{t_i-\tau}^{t_i} eE_{\text{THz}}(t)dt/m_e$, by subtracting these two curves, we gain a direct relationship between

the terahertz electric field strength and the acoustic pressure enhancement:

$$\Delta p(\pi/2) - \Delta p(-\pi/2) \propto \vec{E}_{\text{THz}}. \quad (13)$$

By subtracting the time resolved acoustic curves for these respective phases, both “background” acoustic emission from the dual color plasma and the second order heating term $E_{\text{THz}}(t)^2$ are cancelled, since these are symmetric for the dual-color ionization, leaving only the change in acoustic emission from electron momentum change by the terahertz field prior to the first collision event, after which the electron drift is randomized and its coherence is lost. In Fig. 26(b), the terahertz waveform obtained by subtracting $\Delta p(-\pi/2)$ from $\Delta p(\pi/2)$ is compared to that obtained by an electro-optic crystal. Figure 26(c) compares the spectra of the respective methods performed in air and the agreement between the well documented water vapor absorption line locations, which give further confidence that acoustic emission can be used to encode spectral information of materials; where the spectral resolution is a function of the scan length. Terahertz-wave-enhanced acoustic emission from two-color laser field-induced plasma therefore offers a unique solution for coherent terahertz wave detection, and has potential for use in remote terahertz wave sensing.

3.3 Remote sensing with acoustics

In addition to initial demonstrations of acoustic spectral encoding at short ranges, the feasibility for carrying these acoustic frequencies over larger distances was investigated. Another broadband microphone, (40AC from GRAS with higher sensitivity at the lower frequency range), was placed at the 3 inch¹⁾ focus of a 12 inch parabolic collection dish. The entire assembly was moved to varying radial distances from the plasma source. The humidity in the lab during the experiment was approximately 40%. Figure 27 shows higher frequencies are attenuated after 11 meters of propagation (test limited by lab space), but the acoustic pulses contained reasonable bandwidth up to 40 kHz.

This indicates detection of acoustic frequencies well beyond the human limit (20 kHz) is possible at standoff distances. In another experiment, a member of our team stood directly in front of the plasma source and the acoustic signal was collected from several meters. As shown in Fig. 28(a), the acoustic pulse was detected without having a direct line of sight to the plasma. This could be advantageous if information needed to be collected from around a corner or from a separate room that did not allow a direct line of sight to the plasma detector.

Following the acoustic wave propagation experiments, the acoustic modulation induced by the incident terahertz radiation was tested. Due to the particular arrangement of

1) 1 inch \approx 2.54 cm

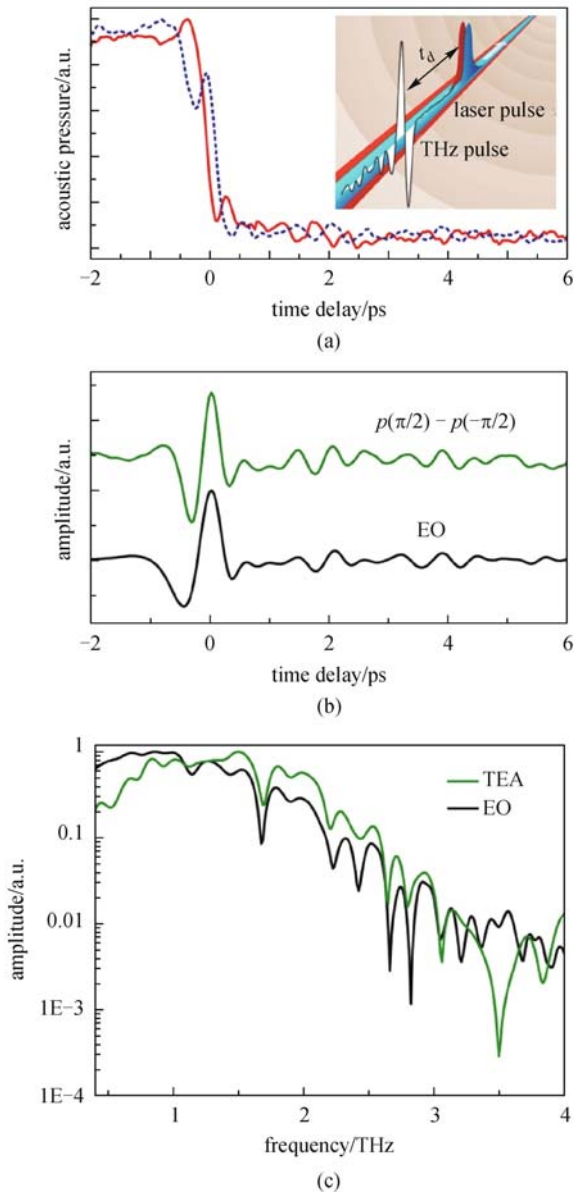


Fig. 26 (a) Acoustic pressure enhancement as a function of time delay t_d at relative phase delay of $\pi/2$ (solid line) and $-\pi/2$ (dashed line). Inset, the experimental schematic of interaction of the terahertz pulse and two-color laser plasma; (b) comparison between the terahertz time-domain waveforms measured by terahertz-wave-enhanced acoustic emission and electro-optic sampling respectively in ambient air; (c) corresponding spectral comparison of the waveforms in (b). TEA; terahertz enhanced acoustics; EO: electro-optic

the experimental setup, the optical pulse energy used to form the acoustic sensor was $100 \mu\text{J}$; an energy only slightly above the ionization threshold needed for plasma formation. At this optical pulse energy level, the plasma is inaudible to the human ear. For this reason, the acoustic signal range was limited to three meters standoff showing 5% modulation, as shown in Fig. 28(b), after 10 averages taken using the 40th harmonic of the laser with a 300 ms time constant.

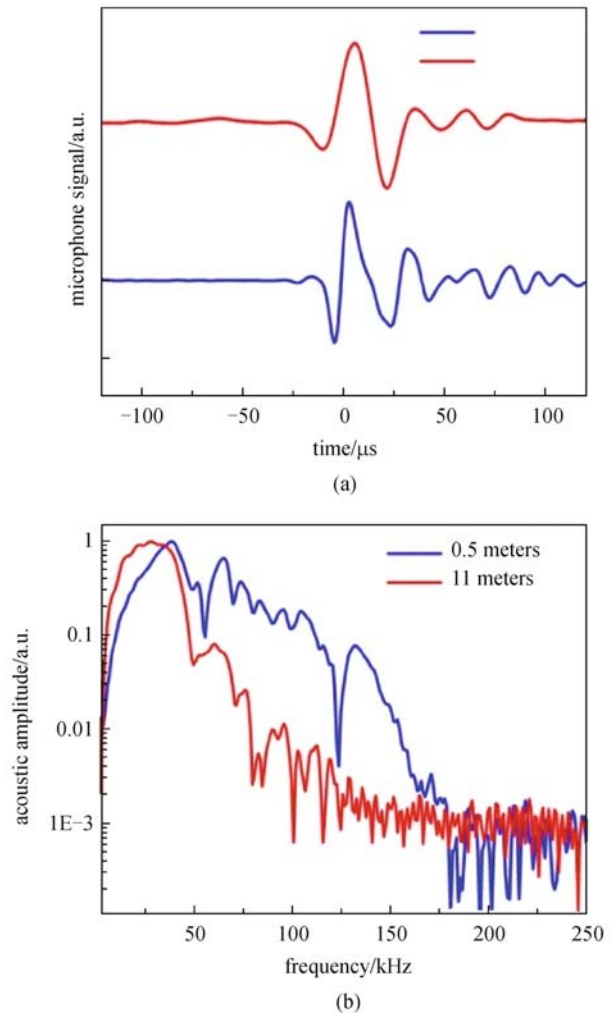


Fig. 27 Temporal and spectral characteristics of acoustic pulses collected using a broadband microphone mounted at the 3 inch focus of a 12 inch diameter parabolic reflector. (a) Normalized temporal pressure transients at 0.5 and 11 meters from the plasma source; (b) normalized spectral comparison of 0.5 and 11 meters acoustic pulse propagation

With an upgrade in the experimental equipment, including higher power optical pulses used for plasma formation, a microphone with higher sensitivities at frequencies, and a larger collection dish used for focusing the acoustic energy onto the microphone, it is expected that the terahertz enhanced acoustic signal could be detected from much greater distances due to large improvements in the system SNR. For example, by using millijoule pulse energies such as those used in Fig. 27, the plasma acoustics are audible from the offices adjacent to the laboratory even with the doors closed.

4 Conclusions

In conclusion, we presented two milestone developments in terahertz wave science and technology geared towards

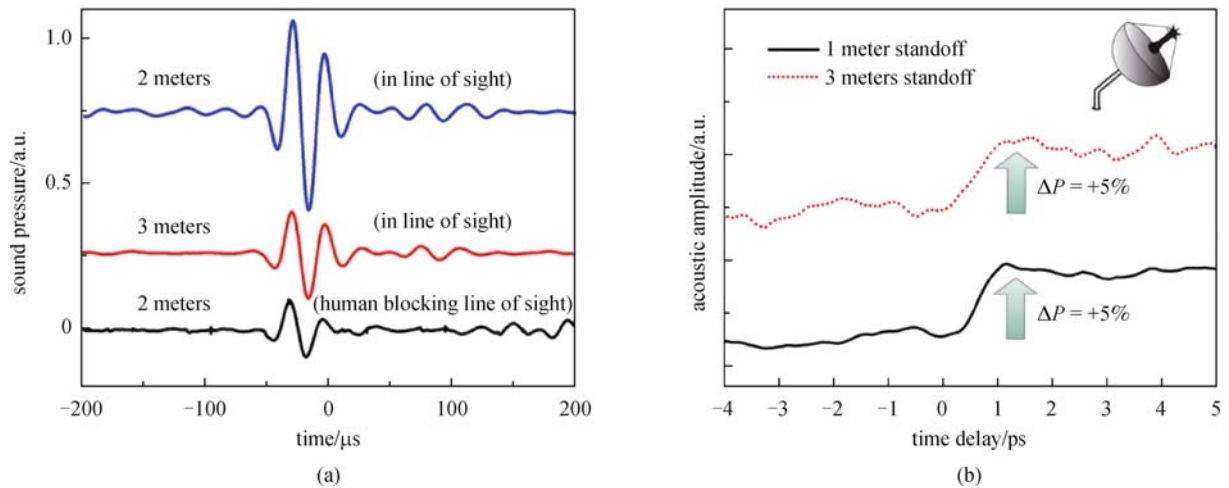


Fig. 28 (a) Acoustic pulses collected with and without direct line of sight to the plasma acoustic source from several meters; (b) terahertz enhanced acoustic signal collected at standoff distance of 1 and 3 meters from the plasma source using a 12" diameter parabolic reflector with the microphone positioned at the 3" focus

coherent detection of terahertz waves using air-based sensors. The photoacoustic and photoluminescent emission, as well as manipulation of electron motion inside a volume of ionized air, were used to overcome existing sensor limitations and extend the useful range of existing terahertz technology. The study will push the development of terahertz field strengths and bandwidths, key applications in spectroscopy, non-invasive evaluation of materials, and imaging.

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